

Design of Parallel-Plate Transmission Line Feeding Differentially Driven Patch Antenna for GPS application

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ABSTRACT

In this paper a newly developed patch antenna, designated as the parallel-plate transmission line feeding differentially driven patch antenna is presented. The parallel-plate transmission line will not introduce inductance to the input impedance of a patch antenna, thus the height of the patch can be largely increased. Measurements show that the 3-dB-gain bandwidth can be obtained to 65% (0.86–1.93 GHz), return loss is -20dB, VSWR is 1.3 and impedance is 51 ohm at resonant frequency of 1.58GHz. The radiation pattern is stable and this antenna is designed for GPS application.

INDEX TERMS

3-dB-gain bandwidth, Differentially driven antenna, bandwidth, parallel-plate transmission line, CADFEKO.



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INTRODUCTION

In Recent years, differential circuits are becoming more popular in microwave circuit design, due to their good performances such as low noise, harmonic suppression, high linearity, and large dynamic range. Thus they can be used in radio frequency integrated circuits (RFICs) and microwave monolithic integrated circuits (MMICs) [1] [2]. However, most antennas are designed for single-ended circuits. Baluns are required to transform differential signals to single-ended signals, when they are integrated with differential circuits. Thus, differentially driven antennas are demanded in differential microwave circuit designs to get rid of bulky off-chip and lossy on-chip baluns to improve the receiver noise performance or transmitter power efficiency. Moreover, the cancellation mechanism introduced by the differentially driven scheme largely reduces the cross-polarization radiation and thus enhances the polarization purity of the antenna [1] [3] [6].

Stable radiation and Wide gain bandwidths are the most demanded features for patch antennas. The easiest way to enhance the 3-dB bandwidth is to increase the height of the patch above the ground plane. However, because of the inductance introduced by the feeding structure, the height of the patch has to be limited within a few percent of a wavelength. For coaxial probe feeding, the height of the probe has to be increased with the height of the patch, which introduces extra inductance to the input impedance and deteriorates the input matching of the antenna. This effect limits the bandwidth of patch antennas [8].

A numerical study of newly developed patch antenna, designated as the parallel plate transmission line feeding differentially driven patch antenna has been presented. The parallel plate transmission line will not introduce inductance to the input impedance of the patch antenna, thus the height of the patch can be largely increased.

ANTENNA DESIGN

A. Electrical Parameters of Differentially Driven Antenna

For symmetric differentially Driven patch antenna, the differential input impedance Z_d is given by [5]

$$Z_{d} = Z_{11} - Z_{12} - Z_{21} - Z_{22} \tag{1}$$

Where Z11, Z12, Z21 and Z_{22} are Z-parameters of two input ports when the differentially driven antenna is regarded as a two port single-ended network. The frequency at which the reactance of the input impedance Z_d is equal to zero is known as resonant frequency [5]. From (1), we achieve the following relation as:

$$S_{d11}=1(S_{11}-S_{12}-S_{21}-S_{22})/2$$
 (2)

Where S_{d11} is the reflection coefficient of differentially driven antenna. S_{11} , S_{12} , S_{21} and S_{22} are S-parameters of two input ports when the differentially driven antenna is regarded as a two port single-ended network. In this paper, the 3-dB gain bandwidth of the differentially driven patch antenna is defined as a range of frequencies over which the differential reflection coefficient is less than 10 dB (S_{d11} <-10 dB).

B. Antenna Design

The basic structure of the proposed antennas consists of a ground plane, a parallel-plate transmission line formed by two parallel plates, and a radiation patch. For conventional single ended probe feeding, the series inductance introduced by the probe is from the self-inductance of the probe. The longer the probe is, the larger the inductance will be introduced. This deteriorates the input matching of the antenna. On the other hand, the connection between the parallel plate and other parts of the antenna will also introduce a reactive component to the input impedance. However, according to the transmission line theory, series distributed inductance and shunt distributed capacitance make the parallel plate becomes a transmission line. From the microwave network theory, we know that the transmission line itself does not introduce a reactive component, but only changes the phase of signals. Thus, no matter how long it is, the parallel plate will not introduce extra inductance to the input impedance. By this way, the height of the patch fed by the parallel plate can be largely increased. Two lower edges of the parallel-plate transmission line are connected to two short feeding probes of two 500hm SMA launchers. The characteristic impedance of the differential feeding line, thus, is 1000hm. The short feeding probes are inevitable, but will only introduce small inductance to the input impedance of the antenna. The two SMA ports below the ground, together, are designated as the "differential input port" of the differentially driven patch antenna in [1].

For the antennas proposed in this paper, the ground plane is made with the thickness of 2 mm. The radiation patch and parallel-plate transmission line are made with the thickness of 0.3 mm. The radii of the two probes are 0.025 mm. First, the parallel-plate transmission line is used to feed the radiation patch directly. This means the two higher edges of the parallel plate are connected to the bottom of the patch. Thus, electromagnetic (EM) energy can be transmitted from the parallel plate to the patch directly



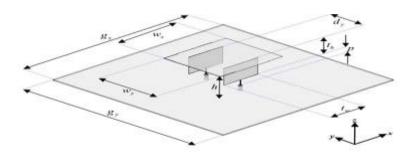


Fig.1 Geometry of Parallel-Plate transmission line, direct-feeding differentially driven patch antenna.

The geometry of the first antenna is shown in Fig. 1, where optimized geometrical parameters of the antenna are also given as shown in table 1.

Table 1

Parameter	$g_x = g_y$	t _w	t _h	р	h	d _y	W _y	W _x
Value(mm)	300	74	32.5	5.5	38	30	100	110

The simulation process has been done through FEKO electromagnetic software which is based on method of movement (MOM). The optimization is done through FEKO simulation software. It was used for optimizing electromagnetic problems. The optimized antennas were determined to have desired resonant frequencies, high gain, and low weight return losses.

The radiation patch is placed over a ground at the height of 38mm.

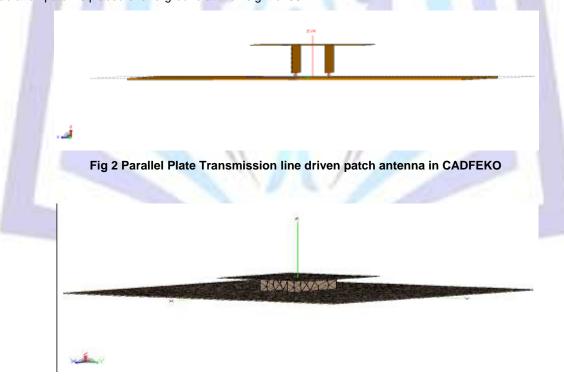
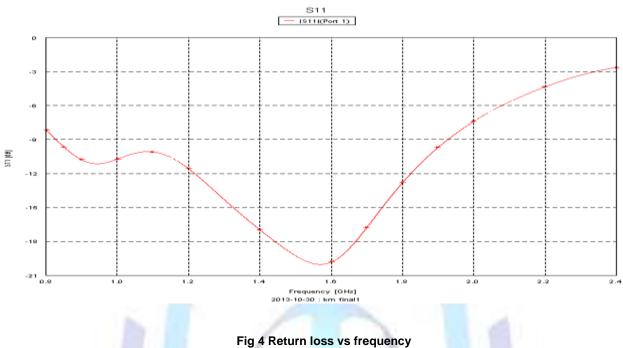


Fig 3 Parallel Plate Transmission line driven patch antenna in POSTFEKO

RESULTS AND ANALYSIS

The simulation process has been done through FEKO electromagnetic software which is based on method of movement (MOM). The 3-dB-gain bandwidth is 65% (0.86–1.93 GHz). It can be observed that the proposed antenna has a Return loss of -20 Db, VSWR is less than 2 and impedance is 51ohmat the resonant frequency of 1.58GHz. It is noted that the resonances occurs at 1.58GHz.





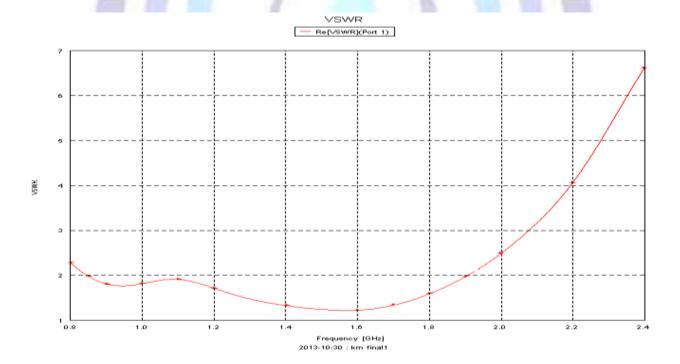


Fig 5 VSWR vs frequency



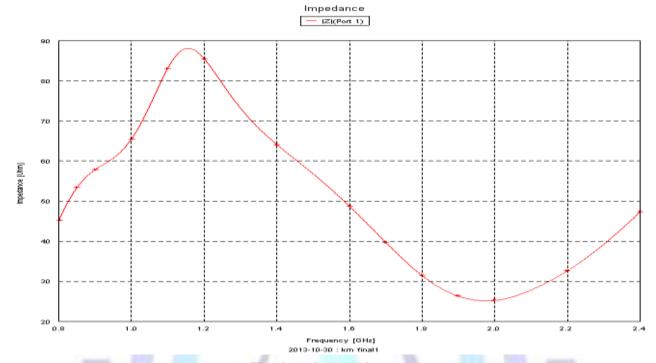


Fig 6 Impedance vs frequency

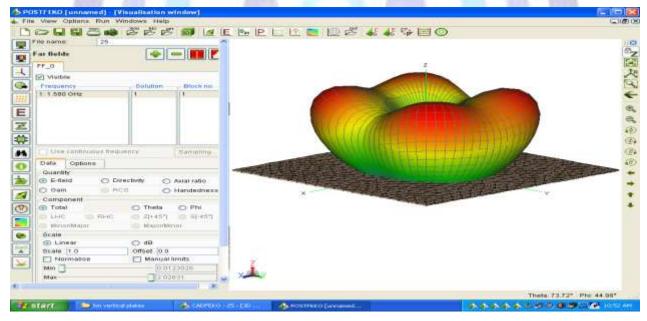


Fig7 3-D view of Radiation Pattern

CONCLUSION

A newly developed single-patch antenna, called parallel-plate transmission line feeding differentially driven patch antenna, has been designed and implemented successfully. The measured results demonstrated that it has a wide 3-dB-gain bandwidth of 65% (0.86–1.93 GHz), return loss is -20dB, VSWR is 1.3 and impedance is 51 ohm at resonant frequency of 1.58GHz. The radiation pattern is stable within the 3-dB-gain bandwidth. Due to the symmetry of the structure and excitation, the radiation pattern is symmetric about both E-plane and H-plane. Due to its wide bandwidth, a possible application of the proposed antenna is that it can be used as a base-station antenna, simultaneously providing different wireless access services, e.g. GPS application.



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